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## Amendments to the Specification:

Please replace the paragraph beginning at page 13, line 17, with the following rewritten paragraph:

Fig. 10 is a cross-sectional view showing an example of a precision sleeve in Fig. 7 onto which a spacer 8 <u>14</u> made of an electric insulation material is interposed.

Please replace the paragraph beginning at page 27, line 11, with the following rewritten paragraph:

The ferrule used for each fiber stub was made of zirconia ceramics. One ferrule sample with the shape shown in Fig. 3 and another ferrule with the shape shown in Fig. 3 15 were obtained by extrusion-molding a ceramic molded object in shape of cylinder hollow, followed by sintering and cutting them.

Please replace the paragraph beginning at page 33, line 1, with the following rewritten paragraph:

The above-mentioned ceramic precision sleeve 4 is preferably made of zirconia with high modulus of elasticity, in light of stress relaxation during attachment and detachment and optimization of press insertion. For approaches of machining the sleeve, a molded object to be the sleeve  $\frac{1}{4}$ , in shape of cylinder or rectangular solid is obtained in advance using a given molding method, such as injection molding, press molding, extrusion molding, and then the molded object is sintered at 1,300 to 1,500 degree-C, followed by cutting or grinding it to predetermined dimensions. Surface roughness of the inner face of the precision sleeve 4 is, in light of insertion, preferably 0.2 µm or below in arithmetic mean roughness (Ra). Tolerances between the outer diameter of the plug ferrule PF and

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the inner diameter of the precision sleeve  $\frac{1}{4}$ , is preferably  $\pm 1$  µm or below to attain lower connection loss.

Please replace the paragraph beginning at page 33, line 19, with the following rewritten paragraph:

Since the ferrule stopper 13 is loaded due to repetition of attachment and detachment of the plug ferrule PF or a continuing spring load of the plug ferrule PF during connection, it requires a sufficient fixing strength. This can be realized by approaches for fixing the ferrule stopper 13 into the precision sleeve  $\frac{1}{4}$  using sufficient press insertion, or adhesives, or combination of press insertion and adhesives.

Please replace the paragraph beginning at page 33, line 28, with the following rewritten paragraph:

The above-mentioned holder 5 is typically welded with a case 22 (See Fig. 12) for an optical module. Therefore, it is made of a weldable material, such as stainless steel, copper, iron, nickel, in particular, stainless steel in light of corrosion resistance and weldability. The metal flange 3 12 is also preferably plated with, e.g., Ni, on the surface or made of stainless steel, in light of corrosion resistance.

Please replace the paragraph beginning at page 37, line 5, with the following rewritten paragraph:

Then, the outer diameter of the fiber stub 1 is 1 to 7 µm larger than the inner diameter of the precision sleeve 4 into which the fiber stub 1 is pressed. Since the precision sleeve 4 and the fiber stub 1 are made of the same material to coincide with each other in thermal expansion coefficient, a grip force of the precision sleeve

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 $\frac{1}{4}$  for securing the fiber stub 1 is not much changed even when ambient temperature is changed.

Please replace the paragraph beginning at page 38, line 10, with the following rewritten paragraph:

For approaches of machining ceramics, in a case of, e.g., zirconia ceramics, a molded object in shape of cylinder or rectangular solid is obtained in advance using a given molding method, such as injection molding, press molding, extrusion molding, and then the molded object is sintered at 1,300 to 1,500 degree-C, followed by cutting or grinding it to predetermined dimensions. Incidentally, the molded object may be cut to predetermined dimensions before sintering. An end face of the fiber stub 4 1 on side of the plug ferrule is machined in a curved shape with a radius of curvature of approximately 5 to 30 mm to reduce connection loss with an optical connector. Another end face on the side of an optical device is mirror finished with a tilted face having approximately 4 to 10 degree to suppress reflected light which has been emitted from the optical device and then reflected by the end face of the optical fiber, and then returned to the optical device.

Please replace the paragraph beginning at page 41, line 3, with the following rewritten paragraph:

Next, the precision sleeve 4 was pressed and fixed into the holder 5, made of SUS304 with good weldability, on the side of the fiber stub 1 being pressed in. This was also pressed in using a handpress equipped with a pressure sensor while confirming a sufficient load. The press insertion load was approximately 130 N around the fixed position of this sample. Next, the flange 3 12 made of resin was pressed in and reinforced using adhesives, resulting in the optical receptacle 7.